

1 **BEFORE THE PUBLIC UTILITIES COMMISSION**  
2 **OF THE STATE OF CALIFORNIA**

3 **REPLY TESTIMONY OF QUALEN CHAVIS IN SUPPORT OF**  
4 **JOINT APPLICATION OF HORIZON WEST TRANSMISSION, LLC (U222E),**  
5 **FORMERLY KNOWN AS NEXTERA ENERGY TRANSMISSION WEST, LLC, AND**  
6 **PACIFIC GAS AND ELECTRIC COMPANY (U39E) FOR PERMITS TO CONSTRUCT**  
7 **THE ESTRELLA SUBSTATION AND PASO ROBLES REINFORCEMENT PROJECT**  
8 **APPLICATION 17-01-023**  
9

10 1. I, Qualen Chavis, offer this testimony in support of the Joint Application of  
11 Horizon West Transmission, LLC (“Horizon West”) and Pacific Gas and Electric Company  
12 (“PG&E”) for Permits to Construct the Estrella Substation and Paso Robles Reinforcement  
13 Project (“Estrella Project”), Application 17-01-023 (the “Application”), submitted to the  
14 California Public Utilities Commission (“CPUC” or “Commission”) on January 25, 2017.

15 2. On September 1, 2023, I submitted Opening Testimony in this proceeding, which  
16 included Exhibit 1 and Exhibit 2 attached thereto, which is incorporated herein by reference.

17 3. I am offering this testimony to respond to the Testimony of James Clark (“Clark”) on  
18 Behalf of California Unions for Reliable Energy, submitted in this proceeding on September  
19 1, 2023. My testimony will address the claim made by Clark that “Neither the FEIR nor the  
20 record contain substantial evidence that EMF will be successfully reduced by 15% or greater at  
21 the utility ROW.” Clark Testimony at 12.

22 4. The CPUC’s EMF Policy set forth in Decision 06-01-042<sup>1</sup> requires utilities to  
23 consider “no-cost” and “low-cost” measures, where feasible, to reduce magnetic field exposure  
24 from new or upgraded utility facilities. The EMF Policy established a benchmark of four percent

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<sup>1</sup> “Order Instituting Rulemaking to update the Commission’s policies and procedures related to electromagnetic fields emanating from regulated utility facilities.” D.06-01-042 (Jan. 26, 2006).

25 of total project costs to implement mitigation measures that achieve incremental magnetic field  
26 reductions of at least 15% at the edge of right-of-way (“ROW”).

27 5. Decision 06-01-042 does not require PG&E to model the magnetic field at the  
28 edge of the ROW; rather it requires PG&E to achieve a reduction of magnetic field strength of  
29 15% at the edge of the ROW as compared to the original design of the project:

30 “Our review of the modeling methodology provided in the utility design  
31 guidelines indicates that it accomplishes its purpose, which is to measure the  
32 relative differences between alternative mitigation measures. Thus, the modeling  
33 indicates relative differences in magnetic field reductions between different  
34 transmission line construction methods, but does not measure actual  
35 environmental magnetic fields. In the same way, these relative differences in  
36 mitigation measures will be evident regardless of whether a maximum peak or a  
37 projected peak is used for the comparisons.  
38

39 It is also true that post construction measurement of EMF in the field cannot  
40 indicate the effectiveness of mitigation measures used as it would be extremely  
41 difficult to eliminate all other EMF sources. We note that ordering EMF field  
42 measurements would lead to arguments regarding the risks associated with  
43 absolute EMF values and an attempt to determine health based standards, an issue  
44 excluded from this proceeding.” (pp. 11-12.)

45 6. As stated in the Final Environmental Impact Report (“FEIR”) prepared by the  
46 CPUC for the Estrella Project (March 2023), “[T]he CPUC does not consider electric and  
47 magnetic fields (EMF) to be an environmental issue in the context of CEQA because there is no  
48 agreement among scientists that EMF creates a potential health risk and because CEQA does not  
49 define or adopt standards for defining any potential risk from EMF and the CPUC’s EMF  
50 Policy.” FEIR at 2-121 et seq.

51 7. As I stated in my Opening Testimony, PG&E applied for a Permit to Construct  
52 (“PTC”) to construct, among other things: (i) the Union Substation; (ii) a new, approximately  
53 7-mile long, double circuit 70 kilovolt (“kV”) line from Union Substation that would connect to  
54 the existing San Miguel-Paso Robles 70 kV line; and (iii) reconductor approximately 3 miles of  
55 the existing San Miguel-Paso Robles 70 kV line from the point at which the new 70 kV line

56 would connect southward to the existing Paso Robles Substation. As a point of clarification, I  
57 note that if it is completed, the Estrella Project would create two new 70 kV circuits: (i) the  
58 Union-San Miguel 70 kV line running from the new Union Substation to the existing San Miguel  
59 Substation; and (ii) the Union-Paso Robles 70 kV line running from the new Union Substation to  
60 the existing Paso Robles Substation. These two 70 kV circuits are configured as a double-circuit  
61 line from Union Substation to the point of connection with the existing San Miguel-Paso Robles  
62 70 kV line. At that point, one of the new 70 kV circuit will be looped into the existing line and  
63 run northward to San Miguel Substation, becoming the new Union-San Miguel 70 kV line. The  
64 other new 70 kV circuit will be looped into the existing line and run southward to San Miguel  
65 Substation, becoming the new Union-Paso Robles 70 kV line.

66 8. As I stated in my Opening Testimony, the Applicants submitted a Preliminary  
67 Field Management Plan as Exhibit E to the Application for the new 70 kV line (“Original Field  
68 Management Plan”), as required by Commission General Order 131-D, Section X(A).

69 9. In March 2023, the Commission issued the FEIR for the Estrella Project that  
70 identified an alternative route for the proposed new 70 kV line as the “environmentally superior”  
71 route, which is referred to in the FEIR as Alternative PLR-1A. Although Alternative PLR-1A  
72 would result in the creation of a new Union-San Miguel 70 kV line and a new Union-Paso  
73 Robles 70 kV line, as requested in the Application, the new double circuit 70 kV line would  
74 traverse a different route and be approximately 3.5 miles longer and require reconductoring of  
75 approximately 3 more miles of the existing San Miguel-Paso Robles 70 kV line.

76 10. It is my understanding that PG&E has determined that the Alternative PLR-1A 70  
77 kV route is the appropriate alignment for the Estrella Project and intends to seek approval from  
78 the Commission to construct it. In support of that determination, PG&E directed me to prepare a

79 Preliminary Field Management Plan for Alternative PLR-1A (“PLR-1A Field Management  
80 Plan”), which I submitted with my Opening Testimony as Exhibit 2. I revised that document,  
81 which is titled the Revised Preliminary Transmission Magnetic Field Management Plan for  
82 Alternative PLR-1A (“Revised PLR-1A Field Management Plan”), and is attached hereto as  
83 Exhibit 1 and incorporated by reference.

84 11. I prepared the Revised PLR-1A Field Management Plan in compliance with the  
85 Commission’s policies governing the mitigation of EMF effects using low-cost and no-cost  
86 measures. The purpose of my testimony is to show how the Revised PLR-1A Field Management  
87 Plan complies with the Commission’s policies.

88 12. Section A.I of the Revised PLR-1A Field Management Plan describes the  
89 transmission lines that will be constructed and/or modified by PG&E for the Estrella Project if  
90 Alternative PLR-1A is constructed. It also includes the estimated total cost of the portion of the  
91 Estrella Project that PG&E will construct, i.e., the transmission line work and the new Union  
92 Substation, which is approximately \$105 million. As it notes, four percent of this estimated total  
93 is \$4.2 million.

94 13. Section A.IV of the Revised PLR-1A Field Management Plan describes the “no  
95 cost” magnetic field reduction measures proposed to be implemented and the incremental  
96 reduction in magnetic field strength achieved at the ROW boundary. Specifically, the measure  
97 proposed is to optimally phase the Union-San Miguel and Union-Paso Robles 70 kV circuits in  
98 the new 10.5 mile double-circuit 70 kV line. A table is presented showing that without optimal  
99 phasing, the “Base Case,” the magnetic field strength would be 94.1 milligauss (“mG”) at each  
100 edge of the ROW (the “North ROW” and “South ROW”), and that with optimal phasing, the  
101 “Optimal Case,” the magnetic field strength would drop to 32.8 mG at each ROW edge. This

102 constitutes a reduction of 65.1%, which is well above the 15% standard required by the CPUC's  
103 EMF Policy.

104 14. I calculated the magnetic field reductions achieved by implementing the "no cost"  
105 measures using a software program called "FIELDS," originally developed by Southern  
106 California Edison. This software is one of several programs available at PG&E to perform the  
107 computer modeling of the magnetic field environment of electric transmission lines. This  
108 program has been used by PG&E and other California utilities to model magnetic field strength  
109 reductions achieved by implementing "no cost" and "low cost" measures.

110 15. Section A.IV also describes the "low cost" magnetic field reduction measures  
111 proposed to be implemented along the new 10.5-mile double circuit 70 kV line. Specifically, the  
112 measure proposed is to raise the conductor height by 10 feet more than required to meet  
113 minimum clearance requirements. A table is presented showing the Base Case magnetic field  
114 strength at each edge of the ROW is 32.8 mG, which is the strength achieved through optimal  
115 phasing (the "no cost" measure described above). By raising the conductor height 10 feet, the  
116 magnetic field drops to 20.3 mG, an additional reduction of 38.2%.

117 16. Exhibit 2, which is attached hereto and incorporated by reference, presents the  
118 input parameters that I used to model the magnetic field strength for the Base Case and Optimal  
119 Phasing for the new 10.5 mile double-circuit 70 kV line in Alternative PLR-1A. Key inputs  
120 found in Table 1 of Exhibit 2 is a ROW width of 30 feet from the centerline. Key inputs in  
121 Table 2 of Exhibit 2 include: current of 975 amperes, minimum conductor height of 29 feet, and  
122 phasing of the three conductors in each 70 kV circuit. Exhibit 2 also includes a diagram  
123 illustrating how the three conductors in each 70 kV circuit are arranged on a double-circuit pole.

124           17.     Exhibit 3, which is attached hereto and incorporated by reference, is a chart of the  
125     output data from the FIELDS software using the data inputs presented in Exhibit 2. It shows the  
126     modeled field strength of the new double-circuit 70 kV line at various distances from the  
127     centerline of the ROW at the base case (no optimal phasing and minimum conductor height),  
128     with optimal phasing, and raising conductor height by 10 feet.

129           18.     Exhibit 4, which is attached hereto and incorporated by reference, presents a  
130     graph of the output data from the FIELDS software using the data inputs presented in Exhibit 3.  
131     The X-axis represents distance from the centerline of the ROW, which is “0” on the X-axis. The  
132     Y-axis represents magnetic field strength. The blue line represents the modeled magnetic field in  
133     the base case at various distances from the ROW centerline. The green line represents the  
134     modeled magnetic field implementing “no cost” optimal phasing at various distances from the  
135     ROW centerline. The red line presents the modeled magnetic field at various distances from the  
136     ROW centerline implementing “no cost” optimal phasing and the “low cost” measure of raising  
137     conductor height by 10 feet. The yellow vertical lines represent a distance of 30 feet from the  
138     ROW centerline. The graph provides a visual representation of the relative, incremental  
139     reduction of magnetic field strength that implementation of the no cost and low cost measures  
140     achieves.

141           19.     Based on the modeling I conducted using the FIELDS software, and as presented  
142     in Section A.IV of the Revised Alternative PLR-1A Field Management Plan, the total reduction  
143     in modeled magnetic field strength at the ROW edge achieved along the new 10.5 mile double-  
144     circuit 70 kV line by implementing “no-cost” and “low cost” measures is 73.8 mg. Compared to  
145     the modeled base case field strength of 94.1 mG without optimal phasing and conductors at the  
146     minimum clearance height, implementing both measures results in a reduction of magnetic field

147 strength at the ROW boundary of 78.4%, which is well above the 15% reduction standard in the  
148 CPUC's EMF Policy.

149         20.     Section A.IV of the Revised Alternative PLR-1A Field Management Plan also  
150 presents the incremental reduction in modeled magnetic field strength resulting from  
151 implementing "low cost" measures along the 6-mile portion of the existing San Miguel-Paso  
152 Robles line that would be recondoctored if Alternative PLR-1A is constructed. This  
153 recondoctored section would be composed of the single circuit portion of the new Union-San  
154 Miguel 70 kV line running northward to the existing San Miguel Substation and the single circuit  
155 portion of the new Union-Paso Robles 70 kV line running southward to existing Paso Robles  
156 Substation. "No cost" measures cannot be implemented along this line because it is a single 70  
157 kV circuit, not a double circuit. The "low cost" measure proposed is to raise the conductor  
158 height by 10 feet more than required to meet minimum clearance requirements. A table is  
159 presented showing the modeled base case (i.e., conductor height at minimum clearance)  
160 magnetic field strength at the western edge of the ROW is 35.5 mG and at the eastern edge of the  
161 ROW is 35.9 mG. By raising the conductor height 10 feet, the modeled magnetic field at the  
162 western edge of the ROW drops to 25.3 mG and drops to 25.7 mG at the eastern edge of the  
163 ROW, a reduction of 28.6% and 28.5% respectively.

164         21.     Exhibit 5, which is attached hereto and incorporated by reference, presents the  
165 input parameters that I used to model the magnetic field strengths for the base case in which the  
166 conductor along the 6-mile portion of the existing single circuit San Miguel-Paso Robles 70 kV  
167 line, which would be recondoctored under Alternative PLR-1A, is at the minimum clearance  
168 height and if raised by 10 feet. The key input found in Table 1 of Exhibit 2 is a ROW width of  
169 30 feet from the centerline. Key inputs in Table 2 of Exhibit 2 include: current of 975 amperes,

170 minimum conductor height of 29 feet, and phasing of the three conductors in the 70 kV circuit.  
171 Exhibit 2 also includes a diagram illustrating how the three conductors in the 70 kV circuit are  
172 arranged on a single-circuit pole.

173 22. Exhibit 6, which is attached hereto and incorporated by reference, is a chart of the  
174 output data from the FIELDS software using the data inputs presented in Exhibit 5. It shows the  
175 modeled field strength of the reconductored 70 kV line at various distances from the centerline  
176 of the ROW at the base case (minimum conductor height) and raising conductor height by 10  
177 feet.

178 23. Exhibit 7, which is attached hereto and incorporated by reference, presents a  
179 graph of the output data from the FIELDS software using the data inputs presented in Exhibit 5.  
180 Similar to Exhibit 4, the X-axis represents distance from the centerline of the ROW, which is “0”  
181 on the X-axis. The Y-axis represent magnetic field strength. The blue line represents the  
182 modeled magnetic field in the base case at various distances from the ROW centerline. The red  
183 line represents the modeled magnetic field implementing the “low cost” measure of raising  
184 conductor height by 10 feet at various distances from the ROW centerline. The yellow vertical  
185 lines represent a distance of 30 feet from the ROW centerline. The graph provides a visual  
186 representation of the relative, incremental reduction of magnetic field strength that  
187 implementation of the low cost measures achieves.

188 24. Based on the modeling I conducted using the FIELDS software, and as presented  
189 in Section A.IV of the Revised Alternative PLR-1A Field Management Plan, the incremental  
190 reduction in modeled magnetic field strength at the ROW edge achieved along the new  
191 approximately 10.5 mile double-circuit 70 kV line by implementing “no-cost” and “low cost”  
192 measures is 78.4%, and the incremental reduction in magnetic field strength achieved by



193 implementing “low cost” measures along the approximately 6 miles of recondoctored line is  
194 between 28.6% and 28.5%. All of these incremental reductions are well above the 15%  
195 reduction standard in the CPUC’s EMF Policy.

196 25. If the Commission grants PG&E a PTC that authorizes PG&E to construct  
197 Alternative PLR-1A, it is my understanding that PG&E will incorporate the Revised PLR-1A  
198 Field Management Plan into the design and construction of that new 70 kV route.

199 Executed on September 15, 2023, at San Ramon, California.

200 /s/  
201 \_\_\_\_\_  
202 QUALEN CHAVIS  
203  
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